

Annex D1

Calibration Certificates for Dust Monitoring Equipment

TSP SAMPLER CALIBRATION CACULATION SPREADSHEET

| Location ID: AM1 Name and Model : TISCH HVS Model TE-5170 | Date of Calibration: 26-Apr-23 Next Calibration Date: 26-Jun-23 Operator: P.F.Yeung | | | | | | | |
|--|--|-------------|----------|---|--|---|----------------------|----------|
| CONDITIONS | | | | | | | | |
| Sea Level Pressure (hpa) Temperature (°C) | <table border="1" style="display: inline-table; vertical-align: middle;"> <tr><td>1016</td></tr> <tr><td>20.0</td></tr> </table> | 1016 | 20.0 | Corrected Pressure (mm Hg) Temperature (K) | <table border="1" style="display: inline-table; vertical-align: middle;"> <tr><td>762.1</td></tr> <tr><td>293</td></tr> </table> | 762.1 | 293 | |
| 1016 | | | | | | | | |
| 20.0 | | | | | | | | |
| 762.1 | | | | | | | | |
| 293 | | | | | | | | |
| CALIBRATION ORIFICE | | | | | | | | |
| Make: Model: Serial#: | <table border="1" style="display: inline-table; vertical-align: middle;"> <tr><td>TISCH</td></tr> <tr><td>TE-5025A</td></tr> <tr><td>2454</td></tr> </table> | TISCH | TE-5025A | 2454 | Qstd Slope Qstd Intercept | <table border="1" style="display: inline-table; vertical-align: middle;"> <tr><td>2.06918</td></tr> <tr><td>-0.04220</td></tr> </table> | 2.06918 | -0.04220 |
| TISCH | | | | | | | | |
| TE-5025A | | | | | | | | |
| 2454 | | | | | | | | |
| 2.06918 | | | | | | | | |
| -0.04220 | | | | | | | | |
| CALIBRATION | | | | | | | | |
| Plate No. | H2O(L) (in) | H2O(R) (in) | H2O (in) | Qstd (m ³ /min) | I (chart) | IC (corrected) | LINEAR REGRESSION | |
| 18 | 5.6 | 5.7 | 11.3 | 1.661 | 56 | 56.57 | Slope= 30.829 | |
| 13 | 4.3 | 4.3 | 8.6 | 1.452 | 51 | 51.52 | Intercept= 6.182 | |
| 10 | 3.2 | 3.2 | 6.4 | 1.255 | 45 | 45.46 | Corr. Coeff.= 0.9976 | |
| 7 | 2.0 | 2.0 | 4.0 | 0.997 | 37 | 37.37 | | |
| 5 | 1.3 | 1.3 | 2.6 | 0.808 | 30 | 30.30 | | |

Calulations:

$Q_{std} = 1/m[\sqrt{H_2O(P_a/P_{std})(T_{std}/T_a)} - b]$

$IC = I[\sqrt{P_a/P_{std}}(T_{std}/T_a)]$

Q_{std} = standard flow rate
 IC = corrected chart response
 I = actual chart response
 m = calibrator Q_{std} slope
 b = calibrator Q_{std} intercept
 T_a = actual temperature during calibration (deg K)
 P_a = actual pressure during calibration (mm Hg)

For subsequent calculation of sampler flow:

$1/m(I)[\sqrt{(298/T_{avg})(P_{avg}/760)}] - b$

m = sampler slope
 b = sampler intercept
 I = chart response
 T_{avg} = daily average temperature
 P_{avg} = daily average pressure

TSP SAMPLER CALIBRATION CACULATION SPREADSHEET

| Location ID: AM2 Name and Model : TISCH HVS Model TE-5170 | Date of Calibration: 26-Apr-23 Next Calibration Date: 26-Jun-23 Operator: P.F.Yeung | | | | | | | |
|--|--|-------------|----------|---|--|---|----------------------|----------|
| CONDITIONS | | | | | | | | |
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| CALIBRATION | | | | | | | | |
| Plate No. | H2O(L) (in) | H2O(R) (in) | H2O (in) | Qstd (m ³ /min) | I (chart) | IC (corrected) | LINEAR REGRESSION | |
| 18 | 6.5 | 6.5 | 13.0 | 1.781 | 55 | 55.56 | Slope= 26.274 | |
| 13 | 5.0 | 5.0 | 10.0 | 1.564 | 50 | 50.51 | Intercept= 9.159 | |
| 10 | 3.5 | 3.5 | 7.0 | 1.312 | 43 | 43.44 | Corr. Coeff.= 0.9970 | |
| 7 | 2.3 | 2.3 | 4.6 | 1.067 | 38 | 38.38 | | |
| 5 | 1.4 | 1.4 | 2.8 | 0.837 | 30 | 30.30 | | |

Calulations:

Qstd = $1/m[\text{Sqrt}(H2O(Pa/Pstd)(Tstd/Ta))-b]$
 IC = $I[\text{Sqrt}(Pa/Pstd)(Tstd/Ta)]$

Qstd = standard flow rate
 IC = corrected chart response
 I = actual chart response
 m = calibrator Qstd slope
 b = calibrator Qstd intercept
 Ta = actual temperature during calibration (deg K)
 Pa = actual pressure during calibration (mm Hg)

For subsequent calculation of sampler flow:

$1/m(I)[\text{Sqrt}(298/Tav)(Pav/760)]-b$

m = sampler slope
 b = sampler intercept
 I = chart response
 Tav = daily average temperature
 Pav = daily average pressure

TSP SAMPLER CALIBRATION CACULATION SPREADSHEET

| Location ID: AM3 Name and Model : TISCH HVS Model TE-5170 | Date of Calibration: 26-Apr-23 Next Calibration Date: 26-Jun-23 Operator: P.F.Yeung | | | | | | | |
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| TE-5025A | | | | | | | | |
| 2454 | | | | | | | | |
| 2.06918 | | | | | | | | |
| -0.04220 | | | | | | | | |
| CALIBRATION | | | | | | | | |
| Plate No. | H2O(L) (in) | H2O(R) (in) | H2O (in) | Qstd (m ³ /min) | I (chart) | IC (corrected) | LINEAR REGRESSION | |
| 18 | 5.6 | 5.6 | 11.2 | 1.654 | 63 | 63.64 | Slope= 27.841 | |
| 13 | 4.3 | 4.2 | 8.5 | 1.444 | 58 | 58.59 | Intercept= 17.667 | |
| 10 | 3.2 | 3.3 | 6.5 | 1.265 | 52 | 52.53 | Corr. Coeff.= 0.9971 | |
| 7 | 2.2 | 2.1 | 4.3 | 1.033 | 45 | 45.46 | | |
| 5 | 1.3 | 1.2 | 2.5 | 0.792 | 40 | 40.40 | | |

Calulations:

$Q_{std} = 1/m[\sqrt{H_2O(P_a/P_{std})(T_{std}/T_a)} - b]$

$IC = I[\sqrt{P_a/P_{std}}(T_{std}/T_a)]$

Q_{std} = standard flow rate
 IC = corrected chart response
 I = actual chart response
 m = calibrator Q_{std} slope
 b = calibrator Q_{std} intercept
 Ta = actual temperature during calibration (deg K)
 Pa = actual pressure during calibration (mm Hg)

For subsequent calculation of sampler flow:

$1/m((I)[\sqrt{(298/T_{avg})(P_{avg}/760)}] - b)$

m = sampler slope
 b = sampler intercept
 I = chart response
 T_{avg} = daily average temperature
 P_{avg} = daily average pressure

| Qstd (m³/min) | IC |
|---------------|----|
| 0.8 | 40 |
| 1.0 | 45 |
| 1.3 | 53 |
| 1.4 | 59 |

TSP SAMPLER CALIBRATION CACULATION SPREADSHEET

| Location ID: AM4 Name and Model : TISCH HVS Model TE-5170 | Date of Calibration: 26-Apr-23 Next Calibration Date: 26-Jun-23 Operator: P.F.Yeung | | | | | | | |
|--|--|-------------|----------|---|--|---|----------------------|----------|
| CONDITIONS | | | | | | | | |
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| TE-5025A | | | | | | | | |
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| 2.06918 | | | | | | | | |
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| CALIBRATION | | | | | | | | |
| Plate No. | H2O(L) (in) | H2O(R) (in) | H2O (in) | Qstd (m3/min) | I (chart) | IC (corrected) | LINEAR REGRESSION | |
| 18 | 6.4 | 6.5 | 12.9 | 1.774 | 58 | 58.59 | Slope= 30.581 | |
| 13 | 5.1 | 5.1 | 10.2 | 1.579 | 52 | 52.53 | Intercept= 4.669 | |
| 10 | 3.4 | 3.4 | 6.8 | 1.293 | 45 | 45.46 | Corr. Coeff.= 0.9973 | |
| 7 | 2.4 | 2.4 | 4.8 | 1.090 | 38 | 38.38 | | |
| 5 | 1.5 | 1.5 | 3.0 | 0.866 | 30 | 30.30 | | |

Calulations:

Qstd = $1/m[\sqrt{H2O(Pa/Pstd)(Tstd/Ta)} - b]$
 IC = $I[\sqrt{Pa/Pstd}(Tstd/Ta)]$

Qstd = standard flow rate
 IC = corrected chart response
 I = actual chart response
 m = calibrator Qstd slope
 b = calibrator Qstd intercept
 Ta = actual temperature during calibration (deg K)
 Pa = actual pressure during calibration (mm Hg)

For subsequent calculation of sampler flow:
 $1/m(I)[\sqrt{(298/Tav)(Pav/760)}] - b$

m = sampler slope
 b = sampler intercept
 I = chart response
 Tav = daily average temperature
 Pav = daily average pressure

TSP SAMPLER CALIBRATION CACULATION SPREADSHEET

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|--|--|-------------|----------|---|--|---|----------------------|----------|
| CONDITIONS | | | | | | | | |
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| CALIBRATION | | | | | | | | |
| Plate No. | H2O(L) (in) | H2O(R) (in) | H2O (in) | Qstd (m ³ /min) | I (chart) | IC (corrected) | LINEAR REGRESSION | |
| 18 | 5.1 | 5.1 | 10.2 | 1.548 | 55 | 54.44 | Slope= 32.147 | |
| 13 | 4.1 | 4.1 | 8.2 | 1.390 | 50 | 49.49 | Intercept= 4.931 | |
| 10 | 2.8 | 2.7 | 5.5 | 1.142 | 43 | 42.56 | Corr. Coeff.= 0.9987 | |
| 7 | 2.0 | 1.9 | 3.9 | 0.965 | 36 | 35.64 | | |
| 5 | 1.2 | 1.1 | 2.3 | 0.746 | 29 | 28.71 | | |

Calulations:

$Q_{std} = 1/m[\sqrt{H_2O(P_a/P_{std})(T_{std}/T_a)} - b]$

$IC = I[\sqrt{P_a/P_{std}}(T_{std}/T_a)]$

Q_{std} = standard flow rate
 IC = corrected chart response
 I = actual chart response
 m = calibrator Q_{std} slope
 b = calibrator Q_{std} intercept
 T_a = actual temperature during calibration (deg K)
 P_a = actual pressure during calibration (mm Hg)

For subsequent calculation of sampler flow:

$1/m(I)[\sqrt{(298/T_{avg})(P_{avg}/760)}] - b$

m = sampler slope
 b = sampler intercept
 I = chart response
 T_{avg} = daily average temperature
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TSP SAMPLER CALIBRATION CACULATION SPREADSHEET

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| CONDITIONS | | | | | | | | |
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| CALIBRATION | | | | | | | | |
| Plate No. | H2O(L) (in) | H2O(R) (in) | H2O (in) | Qstd (m3/min) | I (chart) | IC (corrected) | LINEAR REGRESSION | |
| 18 | 6.1 | 6.0 | 12.1 | 1.684 | 53 | 52.46 | Slope= 26.059 | |
| 13 | 4.5 | 4.4 | 8.9 | 1.448 | 48 | 47.51 | Intercept= 8.709 | |
| 10 | 3.5 | 3.5 | 7.0 | 1.286 | 42 | 41.58 | Corr. Coeff.= 0.9952 | |
| 7 | 2.2 | 2.3 | 4.5 | 1.035 | 35 | 34.65 | | |
| 5 | 1.2 | 1.3 | 2.5 | 0.777 | 30 | 29.70 | | |

Calulations:

$Q_{std} = 1/m[\sqrt{H_2O(Pa/Pstd)(Tstd/Ta)} - b]$

$IC = I[\sqrt{Pa/Pstd}(Tstd/Ta)]$

Q_{std} = standard flow rate
 IC = corrected chart response
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 Ta = actual temperature during calibration (deg K)
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For subsequent calculation of sampler flow:

$1/m((I)[\sqrt{(298/Tav)(Pav/760)}] - b)$

m = sampler slope
 b = sampler intercept
 I = chart response
 Tav = daily average temperature
 Pav = daily average pressure

Flow Rate

| Qstd (m³/min) | IC |
|---------------|----|
| 0.8 | 30 |
| 1.0 | 35 |
| 1.7 | 53 |

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| CALIBRATION | | | | | | | | |
| Plate No. | H2O(L) (in) | H2O(R) (in) | H2O (in) | Qstd (m ³ /min) | I (chart) | IC (corrected) | LINEAR REGRESSION | |
| 18 | 5.3 | 5.3 | 10.6 | 1.578 | 60 | 59.39 | Slope= 29.708 | |
| 13 | 4.6 | 4.5 | 9.1 | 1.464 | 54 | 53.45 | Intercept= 11.211 | |
| 10 | 3.4 | 3.4 | 6.8 | 1.268 | 49 | 48.50 | Corr. Coeff.= 0.9953 | |
| 7 | 2.2 | 2.2 | 4.4 | 1.024 | 42 | 41.58 | | |
| 5 | 1.3 | 1.2 | 2.5 | 0.777 | 35 | 34.65 | | |

Calulations:

Qstd = $1/m[\sqrt{H2O(Pa/Pstd)(Tstd/Ta)} - b]$
 IC = $I[\sqrt{Pa/Pstd}(Tstd/Ta)]$

Qstd = standard flow rate
 IC = corrected chart response
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For subsequent calculation of sampler flow:

$1/m(I)[\sqrt{(298/Tav)(Pav/760)}] - b$

m = sampler slope
 b = sampler intercept
 I = chart response
 Tav = daily average temperature
 Pav = daily average pressure

Flow Rate

| Qstd (m ³ /min) | IC |
|----------------------------|-------|
| 0.80 | 34.65 |
| 1.02 | 41.58 |
| 1.26 | 48.50 |
| 1.46 | 53.45 |
| 1.57 | 59.39 |

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| CALIBRATION | | | | | | | | |
| Plate No. | H2O(L) (in) | H2O(R) (in) | H2O (in) | Qstd (m3/min) | I (chart) | IC (corrected) | LINEAR REGRESSION | |
| 18 | 6.1 | 6.1 | 12.2 | 1.691 | 57 | 56.42 | Slope= 31.719 | |
| 13 | 4.6 | 4.5 | 9.1 | 1.464 | 51 | 50.48 | Intercept= 3.367 | |
| 10 | 3.6 | 3.6 | 7.2 | 1.304 | 45 | 44.54 | Corr. Coeff.= 0.998 | |
| 7 | 2.2 | 2.2 | 4.4 | 1.024 | 37 | 36.63 | | |
| 5 | 1.4 | 1.4 | 2.8 | 0.821 | 29 | 28.71 | | |

Calulations:

$Q_{std} = 1/m[\sqrt{H_2O(P_a/P_{std})(T_{std}/T_a)} - b]$

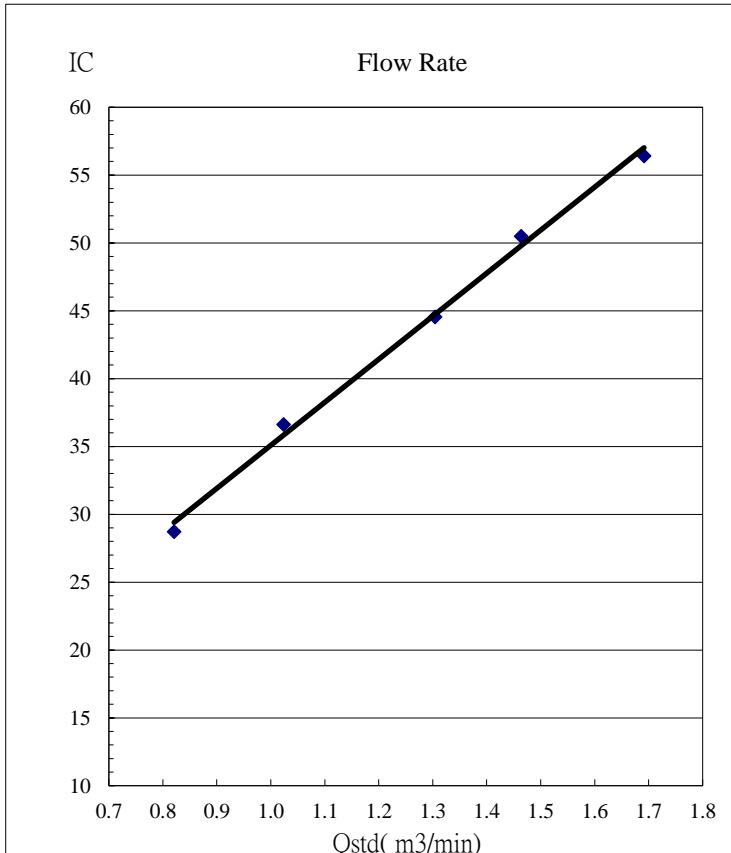
$IC = I[\sqrt{P_a/P_{std}}(T_{std}/T_a)]$

Q_{std} = standard flow rate
 IC = corrected chart response
 I = actual chart response
 m = calibrator Q_{std} slope
 b = calibrator Q_{std} intercept
 T_a = actual temperature during calibration (deg K)
 P_a = actual pressure during calibration (mm Hg)

For subsequent calculation of sampler flow:

$1/m(I)[\sqrt{(298/T_{avg})(P_{avg}/760)}] - b$

m = sampler slope
 b = sampler intercept
 I = chart response
 T_{avg} = daily average temperature
 P_{avg} = daily average pressure



| Qstd (m3/min) | IC |
|---------------|-------|
| 0.821 | 28.71 |
| 1.024 | 36.63 |
| 1.304 | 44.54 |
| 1.464 | 50.48 |